

A new approach to turbulent internal flows with high Reynolds numbers

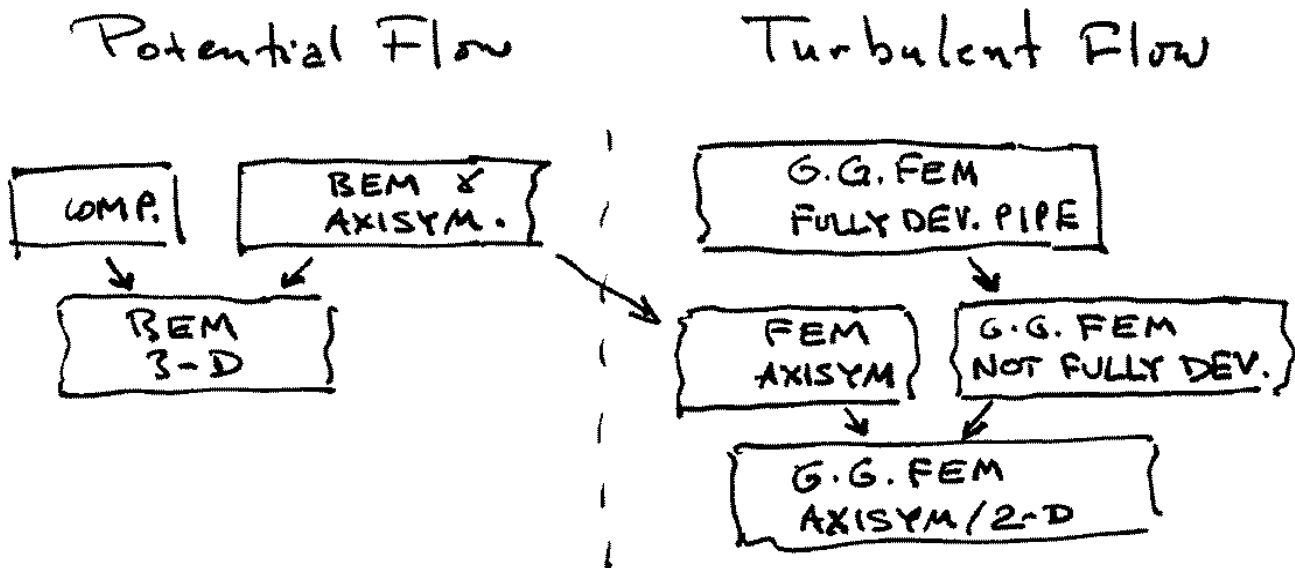
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The authors have developed a method for fast and extremely accurate computation of axisymmetric or two-dimensional internal turbulent flows with Reynolds number between 10^7 and 10^8 . The main ingredients are a modification of the Galerkin method based on splining (to overcome difficulties of the standard Galerkin method at the boundary) and a curvilinear orthogonal coordinate system following the boundary and approximately following the flow lines. I will describe the two techniques and present some applications.



A. Gokhman, *Determination of the axisymmetric potential flow in the passages of turbomachines using the method of singularities*, *Computation of Internal Flows: Methods and Applications*, FED 14:137-149 (1983)

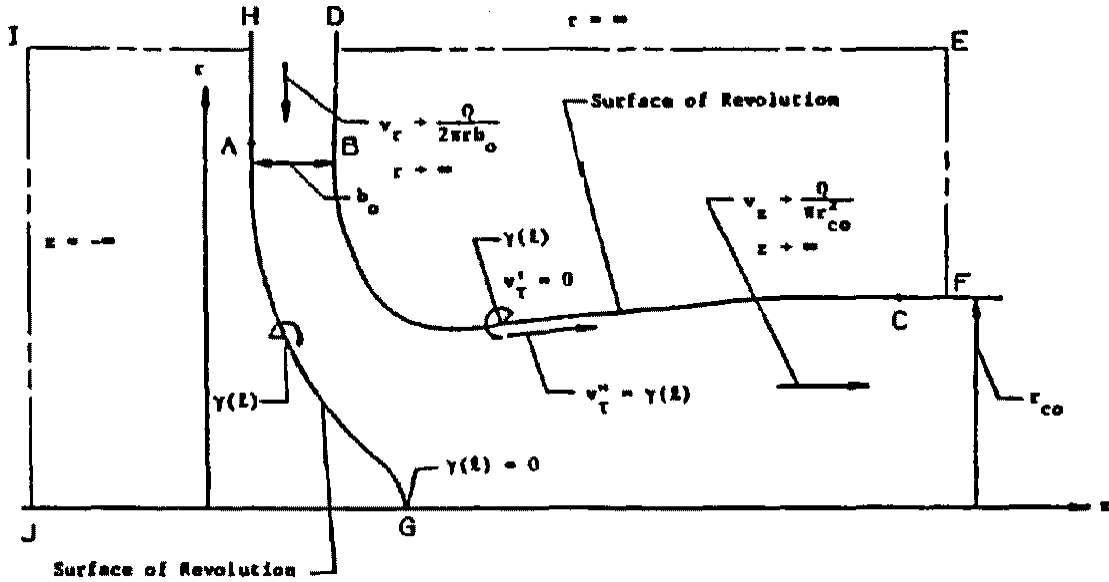
A. Gokhman, *New method for solving partial and ordinary differential equations using finite-element technique*, *Numerical Heat Transfer, Part B* 18:1-22 (1990)

D. Gokhman, *Computation of the velocity field due to vortex filaments in a fluid passage*, *Fluid & Power Research Institute, Tech. Rep.* 1-22 (1991)

A. Gokhman, D. Gokhman, *A highly accurate method for axisymmetric flow*, *Mathematical Problems in Engineering*, 1:11-25 (1995)

A. Gokhman, D. Gokhman, *Boundary element method for axisymmetric flow*, In preparation

Boundary Element Method for Axisymmetric Flow



Governing equation: $\nabla^2 \varphi = 0$

$$\frac{\partial^2 \varphi}{\partial z^2} + \frac{1}{r} \frac{\partial \varphi}{\partial r} + \frac{\partial^2 \varphi}{\partial r^2} = 0, \quad v_r = \frac{\partial \varphi}{\partial r}, \quad v_z = \frac{\partial \varphi}{\partial z}, \quad v_\theta = 0$$

Boundary conditions:

(a) Radial with distance between the planes b_0 : $v_z \prec v_r \sim \pm \frac{Q}{2\pi r b_0}$ as $r \rightarrow \infty$

(b) Cylinder with radius r_0 : $v_r \rightarrow 0, v_z \rightarrow \pm \frac{Q}{\pi r_0^2}$ as $z \rightarrow \pm\infty$,

(c) Cone with vertex $(0, z_0)$ and generatrix $r = \tan \alpha (z - z_0)$:

$$\mathbf{v}(r, z) \sim \pm \frac{Q}{2\pi(1 - \cos \alpha) |\mathbf{n}|^3} \mathbf{n}, \text{ as } |\mathbf{n}| \rightarrow \infty, \text{ where } \mathbf{n} = (r, z - z_0).$$

$$\frac{\gamma}{2} = \frac{dr}{d\ell} u_r + \frac{dz}{d\ell} u_z$$

$$u_r = \frac{1}{4\pi} \int_{\mathcal{L}} \gamma(\ell) r(\ell) (z_c - z(\ell)) \int_0^{2\pi} \frac{\sin \theta}{(r(\ell)^2 + r_c^2 - 2r_c r(\ell) \sin \theta + (z_c - z(\ell))^2)^{\frac{3}{2}}} d\theta d\ell$$

$$u_z = \frac{1}{4\pi} \int_{\mathcal{L}} \gamma(\ell) r(\ell) \int_0^{2\pi} \frac{r(\ell) - r_c \sin \theta}{(r(\ell)^2 + r_c^2 - 2r_c r(\ell) \sin \theta + (z_c - z(\ell))^2)^{\frac{3}{2}}} d\theta d\ell$$

(a) Radial: $\gamma \sim \pm \frac{Q}{2\pi b_0 r}$ as $r \rightarrow \infty$ with opposite signs on the two planes.

(b) Cylinder: $\gamma \rightarrow \pm \frac{Q}{\pi r_0^2}$ as $z \rightarrow \pm\infty$

(c) Cone: $\gamma \sim \pm \frac{Q}{2\pi(1 - \cos \alpha) |\mathbf{n}|^2}$ as $|\mathbf{n}| \rightarrow \infty$, where $\mathbf{n} = (r, z - z_0)$

We can compute the integrals with respect to $d\ell$ exactly using the following table integrals

$$\begin{aligned}
T_n &= \int \frac{\ell^n d\ell}{(\ell^2 + b\ell + a)^{\frac{3}{2}}} \quad [n = 0, 1, -1] \\
T_0 &= \frac{2(2\ell + b)}{(4a - b^2)(\ell^2 + b\ell + a)^{\frac{1}{2}}} \quad T_1 = -\frac{2(2a + b\ell)}{(4a - b^2)(\ell^2 + b\ell + a)^{\frac{1}{2}}} \\
T_2 &= -2 \frac{(3a - b^2)\ell - ab}{(4a - b^2)(4a - b^2)(\ell^2 + b\ell + a)^{\frac{1}{2}}} + \ln \left(2(\ell^2 + b\ell + a)^{\frac{1}{2}} + 2\ell + b \right) \\
T_3 &= \frac{(4a - b^2)\ell^2 + b(10a - 3b^2)\ell + a(8a - 3b^2)}{(4a - b^2)(\ell^2 + b\ell + a)^{\frac{1}{2}}} - \frac{3b}{2} \ln \left(2(\ell^2 + b\ell + a)^{\frac{1}{2}} + 2\ell + b \right) \\
T_{-1} &= -\frac{2(b\ell - 2a + b^2)}{a(4a - b^2)(\ell^2 + b\ell + a)^{\frac{1}{2}}} - \frac{1}{a^{\frac{3}{2}}} \ln \left(\frac{2a + b\ell + 2a^{\frac{1}{2}}(\ell^2 + b\ell + a)^{\frac{1}{2}}}{\ell} \right)
\end{aligned}$$

and their definite forms

$$\begin{aligned}
T_n^* &= \int_{\ell_0}^{\infty} \frac{\ell^n d\ell}{(\ell^2 + b\ell + a)^{\frac{3}{2}}} = \lim_{\ell \rightarrow \infty} T_n(\ell) - T_n(\ell_0) \quad [n = 0, 1, -1] \\
T_0^* &= \frac{2}{4a - b^2} \left(2 - \frac{2\ell_0 + b}{(\ell_0^2 + b\ell_0 + a)^{\frac{1}{2}}} \right) \quad T_1^* = \frac{2}{4a - b^2} \left(\frac{2a + b\ell_0}{(\ell_0^2 + b\ell_0 + a)^{\frac{1}{2}}} - b \right) \\
T_{-1}^* &= \frac{2}{a(4a - b^2)} \left(\frac{b\ell_0 - 2a + b^2}{(\ell_0^2 + b\ell_0 + a)^{\frac{1}{2}}} - b \right) + \frac{1}{a^{\frac{3}{2}}} \ln \left(\frac{2a + b\ell_0 + 2a^{\frac{1}{2}}(\ell_0^2 + b\ell_0 + a)^{\frac{1}{2}}}{(b + 2a^{\frac{1}{2}})\ell_0} \right)
\end{aligned}$$

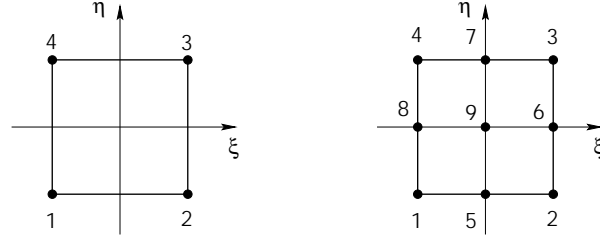
Radial: $r(\ell) = \ell$, $\ell > \ell_0$, $z = z_0$

$$a = r_c^2 + (z_c - z_0)^2, \quad b = -2r_c \sin \theta$$

$$\begin{aligned}
u_r &= \pm \frac{Q}{8\pi^2 b_0} \int_0^{2\pi} \int_{\ell_0}^{\infty} \frac{(z_c - z_0) \sin \theta}{(\ell^2 + r_c^2 - 2r_c \ell \sin \theta + (z_c - z_0)^2)^{\frac{3}{2}}} d\ell d\theta \\
&= \pm \frac{Q}{8\pi^2 b_0} \int_0^{2\pi} (z_c - z_0) \sin \theta T_0^* d\theta \\
&= \pm \frac{Q}{8\pi^2 b_0} \int_0^{2\pi} \frac{(z_c - z_0) \sin \theta d\theta}{(z_c - z_0)^2 + r_c^2 \cos^2 \theta} \left(1 - \frac{\ell_0 - r_c \sin \theta}{(\ell_0^2 + r_c^2 - 2r_c \ell_0 \sin \theta + (z_c - z_0)^2)^{\frac{1}{2}}} \right) \\
u_z &= \pm \frac{Q}{8\pi^2 b_0} \int_0^{2\pi} \int_{\ell_0}^{\infty} \frac{\ell - r_c \sin \theta}{(\ell^2 + r_c^2 - 2r_c \ell \sin \theta + (z_c - z_0)^2)^{\frac{3}{2}}} d\ell d\theta \\
&= \pm \int_0^{2\pi} (T_1^* - r_c \sin \theta T_0^*) d\theta \\
&= \pm \int_0^{2\pi} \frac{d\theta}{(\ell_0^2 + r_c^2 - 2r_c \ell_0 \sin \theta + (z_c - z_0)^2)^{\frac{1}{2}}}
\end{aligned}$$

Finite elements with closed form Galerkin integrals

To implement the finite element scheme we will use the following master elements in dimensionless variables ξ and η : 4-node element with bilinear tensor Lagrangian interpolating shape functions for pressure and 9-node element for biquadratic tensor Lagrange interpolating shape functions for velocity as illustrated in the following figure and tables.



Master elements in dimensionless variables ξ and η

Deg.	Nodes	Polynomials
n	$\{t_k: 1 \leq k \leq n\}$	$l_{ni} = \prod_{1 \leq k \leq n, k \neq i} \frac{x - t_k}{t_i - t_k}$
1	$\{-1, 1\}$	$l_{11}(x) = \frac{1}{2}(1 - x)$ $l_{12}(x) = \frac{1}{2}(1 + x)$
2	$\{-1, 0, 1\}$	$l_{21}(x) = \frac{1}{2}x(x - 1)$ $l_{22}(x) = 1 - x^2$ $l_{23}(x) = \frac{1}{2}x(x + 1)$

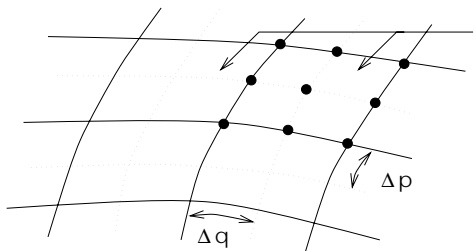
Lagrange interpolating polynomials

$$\begin{aligned} \hat{\varphi}_1(\xi, \eta) &= l_{11}(\xi)l_{11}(\eta) & \hat{\varphi}_2(\xi, \eta) &= l_{12}(\xi)l_{11}(\eta) \\ \hat{\varphi}_3(\xi, \eta) &= l_{12}(\xi)l_{12}(\eta) & \hat{\varphi}_4(\xi, \eta) &= l_{11}(\xi)l_{12}(\eta) \end{aligned}$$

Bilinear tensor Lagrange shape functions for the 4-node element

$$\begin{aligned} \hat{\psi}_1(\xi, \eta) &= l_{21}(\xi)l_{21}(\eta) & \hat{\psi}_2(\xi, \eta) &= l_{23}(\xi)l_{21}(\eta) & \hat{\psi}_3(\xi, \eta) &= l_{23}(\xi)l_{23}(\eta) \\ \hat{\psi}_4(\xi, \eta) &= l_{21}(\xi)l_{23}(\eta) & \hat{\psi}_5(\xi, \eta) &= l_{22}(\xi)l_{21}(\eta) & \hat{\psi}_6(\xi, \eta) &= l_{23}(\xi)l_{22}(\eta) \\ \hat{\psi}_7(\xi, \eta) &= l_{22}(\xi)l_{23}(\eta) & \hat{\psi}_8(\xi, \eta) &= l_{21}(\xi)l_{22}(\eta) & \hat{\psi}_9(\xi, \eta) &= l_{22}(\xi)l_{22}(\eta) \end{aligned}$$

Biquadratic tensor Lagrange shape functions for the 9-node element



Transformed elements

$$\begin{aligned} \text{Elements} \quad p_i &= p_{i-1} + \Delta p & p_{i+1} &= p_i + \Delta p \\ q_i &= q_{i-1} + \Delta q & q_{i+1} &= q_i + \Delta q \\ \xi &= \frac{p - p_i}{\Delta p} \quad (-1 \leq \xi \leq 1) & \eta &= \frac{q - q_i}{\Delta q} \quad (-1 \leq \eta \leq 1) \end{aligned}$$

The relationship between p, q and ξ, η

The governing equations for incompressible steady two-dimensional flow are the conservation of mass (continuity) equation

$$\nabla \cdot \mathbf{v} = 0$$

and the balance of momentum (Navier-Stokes) equation

$$\frac{1}{2} \nabla (|\mathbf{v}|^2) - \mathbf{v} \times (\nabla \times \mathbf{v}) = \mathbf{F} - \frac{1}{\rho} \nabla P + (\nu + \tau) \nabla^2 \mathbf{v},$$

where

- ρ mass density
- \mathbf{v} velocity
- \mathbf{F} body force density
- P pressure
- ν Newtonian kinematic viscosity
- τ turbulent kinematic viscosity

The governing equations written in curvilinear orthogonal coordinates p and q in the two-dimensional are

$$\frac{\partial (h_q v_p)}{\partial p} + \frac{\partial (h_p v_q)}{\partial q} = 0 \quad (1)$$

$$\begin{aligned} \frac{1}{h_p} \left[v_p \frac{\partial v_p}{\partial p} + v_q \frac{\partial v_q}{\partial p} \right] - \frac{v_q}{h_p h_q} \left[\frac{\partial (h_q u_q)}{\partial p} - \frac{\partial (h_p u_p)}{\partial q} \right] &= F_p - \frac{1}{\rho h_p} \frac{\partial P}{\partial p} \\ &+ \frac{\nu + \tau}{h_p h_q} \left[\frac{\partial}{\partial p} \left(\frac{h_q}{h_p} \frac{\partial v_p}{\partial p} \right) + \frac{\partial}{\partial q} \left(\frac{h_p}{h_q} \frac{\partial v_p}{\partial q} \right) \right], \end{aligned} \quad (2)$$

$$\begin{aligned} \frac{1}{h_q} \left[v_q \frac{\partial v_q}{\partial q} + v_p \frac{\partial v_p}{\partial q} \right] + \frac{v_p}{h_p h_q} \left[\frac{\partial (h_p u_p)}{\partial q} - \frac{\partial (h_q u_q)}{\partial p} \right] &= F_q - \frac{1}{\rho h_q} \frac{\partial P}{\partial q} \\ &+ \frac{\nu + \tau}{h_p h_q} \left[\frac{\partial}{\partial p} \left(\frac{h_q}{h_p} \frac{\partial v_q}{\partial p} \right) + \frac{\partial}{\partial q} \left(\frac{h_p}{h_q} \frac{\partial v_q}{\partial q} \right) \right], \end{aligned} \quad (3)$$

where v_p and v_q are the components of \mathbf{v} , F_p and F_q are the components of \mathbf{F} , and h_p and h_q are the metrical coefficients (Lamé functions).

$$\tilde{P} = \sum_{k=1}^4 \hat{\varphi}_k P_k \quad \tilde{v}_p = \sum_{k=1}^9 \hat{\psi}_k v_{pk} \quad \tilde{v}_q = \sum_{k=1}^9 \hat{\psi}_k v_{qk}$$

Continuity equation residual:

$$R_c(v_{pk}, v_{qk}) = \sum_k \left(\frac{\partial h_q}{\partial p} \psi_k + h_q \frac{\partial \psi_k}{\partial p} \right) v_{pk} + \left(\frac{\partial h_p}{\partial q} \psi_k + h_p \frac{\partial \psi_k}{\partial q} \right) v_{qk}$$

$$\langle R_c, \varphi_j \rangle = \sum_k \left(\left\langle \frac{\partial h_q}{\partial p} \psi_k, \varphi_j \right\rangle + \left\langle h_q \frac{\partial \psi_k}{\partial p}, \varphi_j \right\rangle \right) v_{pk} + \left(\left\langle \frac{\partial h_p}{\partial q} \psi_k, \varphi_j \right\rangle + \left\langle h_p \frac{\partial \psi_k}{\partial q}, \varphi_j \right\rangle \right) v_{qk}$$

where

$$\langle f, g \rangle = \iint fg h_p h_q dp dq$$

Spline, e.g.:

$$\begin{aligned} \frac{\partial h_q}{\partial p} h_p h_q &= s(\lambda, \mu) = \sum_{i=1}^{12} s_i \hat{\omega}_i = s(0, 0) \hat{\omega}_1 + s(1, 0) \hat{\omega}_2 + s(1, 1) \hat{\omega}_3 + s(0, 1) \hat{\omega}_4 \\ &+ \frac{\partial s}{\partial p}(0, 0) \Delta p \hat{\omega}_5 + \frac{\partial s}{\partial p}(1, 0) \Delta p \hat{\omega}_6 + \frac{\partial s}{\partial p}(1, 1) \Delta p \hat{\omega}_7 + \frac{\partial s}{\partial p}(0, 1) \Delta p \hat{\omega}_8 \\ &+ \frac{\partial s}{\partial q}(0, 0) \Delta q \hat{\omega}_9 + \frac{\partial s}{\partial q}(1, 0) \Delta q \hat{\omega}_{10} + \frac{\partial s}{\partial q}(1, 1) \Delta q \hat{\omega}_{11} + \frac{\partial s}{\partial q}(0, 1) \Delta q \hat{\omega}_{12} \end{aligned}$$

where

$$\begin{aligned} \hat{\omega}_1(\lambda, \mu) &= H_{01}(\lambda) H_{01}(\mu) & \hat{\omega}_2(\lambda, \mu) &= H_{02}(\lambda) H_{01}(\mu) & \hat{\omega}_3(\lambda, \mu) &= H_{02}(\lambda) H_{02}(\mu) \\ \hat{\omega}_4(\lambda, \mu) &= H_{01}(\lambda) H_{02}(\mu) & \hat{\omega}_5(\lambda, \mu) &= H_{11}(\lambda) H_{01}(\mu) & \hat{\omega}_6(\lambda, \mu) &= H_{12}(\lambda) H_{01}(\mu) \\ \hat{\omega}_7(\lambda, \mu) &= H_{12}(\lambda) H_{02}(\mu) & \hat{\omega}_8(\lambda, \mu) &= H_{11}(\lambda) H_{02}(\mu) & \hat{\omega}_9(\lambda, \mu) &= H_{01}(\lambda) H_{11}(\mu) \\ \hat{\omega}_{10}(\lambda, \mu) &= H_{02}(\lambda) H_{11}(\mu) & \hat{\omega}_{11}(\lambda, \mu) &= H_{02}(\lambda) H_{12}(\mu) & \hat{\omega}_{12}(\lambda, \mu) &= H_{01}(\lambda) H_{12}(\mu) \end{aligned}$$

where λ and μ are shifts of ξ and η and H 's are Hermite interpolant polynomials:

$$\begin{aligned} H_{01}(x) &= 1 - 3x^2 + 2x^3 & H_{02}(x) &= 3x^2 - 2x^3 \\ H_{11}(x) &= x - 2x^2 + x^3 & H_{12}(x) &= -x^2 + x^3 \end{aligned}$$

Top left: $\lambda = \xi + 1$ and $\mu = \eta$

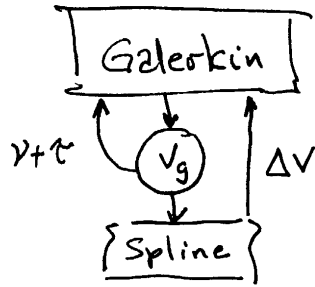
$$\iint \hat{\omega}_7 \hat{\psi}_2 \hat{\varphi}_1 dp dq = \frac{\Delta p \Delta q}{16} \int_0^1 \int_{-1}^0 \left(-\xi^6 - 2\xi^5 + 2\xi^3 + \xi^2 \right) \left(2\eta^6 - 7\eta^5 + 8\eta^4 - 3\eta^3 \right) d\xi d\eta = -\frac{13\Delta p \Delta q}{282240}$$

The Galerkin-Gokhman method

$$v_{pg} = \sum_k \psi_k v_{pk} \quad v_{qg} = \sum_k \psi_k v_{qk} \quad \Delta v_p = v_{ps} - v_{pg} \quad \Delta v_q = v_{qs} - v_{qg}$$

where v_{ps} and v_{qs} are splined.

$\vec{v} + \Delta \vec{v} \rightarrow$ eqs.
Modified continuity eq:



$$\frac{\partial (h_q v_p)}{\partial p} + \frac{\partial (h_p v_q)}{\partial q} = - \frac{\partial (h_q \Delta v_p)}{\partial p} - \frac{\partial (h_p \Delta v_q)}{\partial q}$$

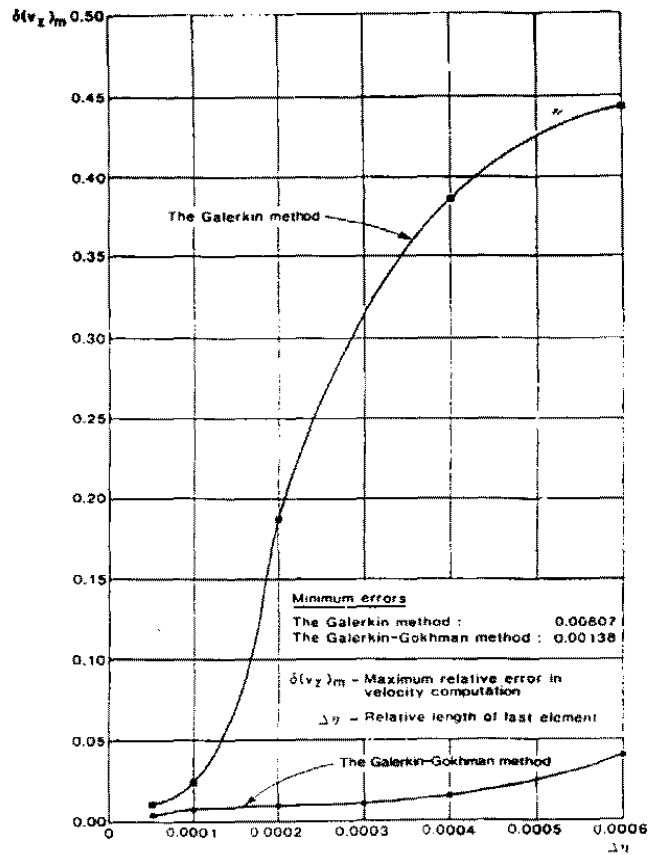
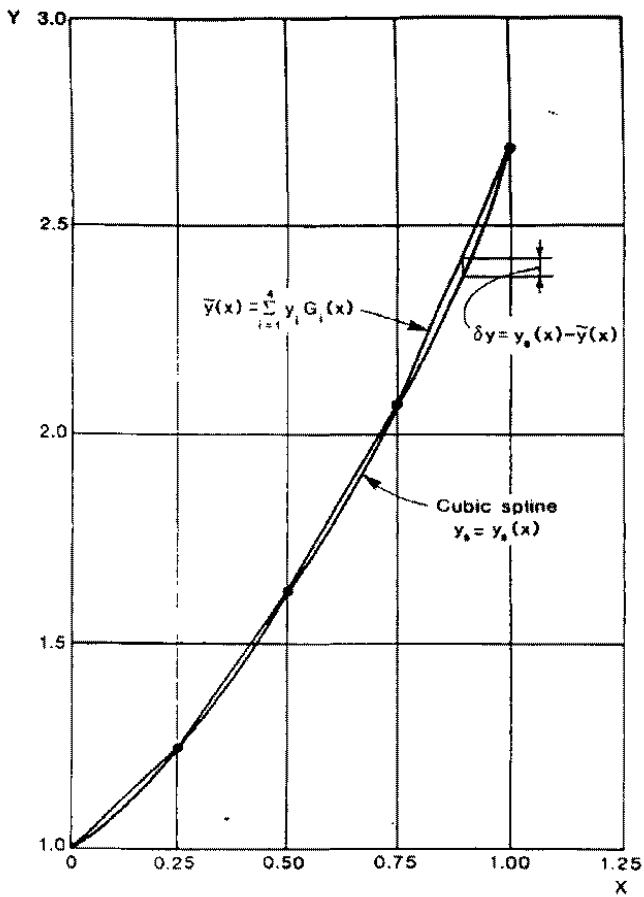


Fig. 2 Parametric study of accuracy of solution for equation describing fully developed flow in a pipe using Galerkin and Galerkin-Gokhman methods at $Re = 10^7$